Target Detection in Sea-Clutter Using Stationary Wavelet Transforms

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Introduction

- Proposed Method: Wavelet Transforms
- Ingara Data Sets
- SWT Experimental Results
 - 5 Detection Performance



Detection Problems

What are the challenges?

- Small target
- Interferences

Sea-spike: strong returned power in time caused by breaking waves on top of sea-surface.

- Breaking waves lasting for a short time before dying out.
- Other persisting on the order of seconds.



Discrete Wavelet Transform

Discrete wavelet transform (DWT) using two sets of filters:

$$A_k(n) = \sum_{m \in z} h_a(2n-m)A_{k-1},$$

$$D_k(n) = \sum_{m \in z} g_a(2n-m)A_{k-1}$$

where h_a and g_a are the analysis low- and high-pass filters. A_k and D_k are the approximate and detail sub-bands at *k*-level.

• Multi-resolution analysis (MRA):



Stationary wavelet transforms (SWT) are used for the investigation.

- No decimation: Avoids artefacts from aliasing when reconstructing subbands because SWT is shift-invariance, the advantage over the DWT.
- MRA: Filter is upsampled at each level, thereby maintain multi-resolution as in DWT.
- Perfect reconstruction.



Subband Isolation and Reconstruction

- Apply SWT along the slow time domain using Daubechies 4 mother wavelet.
- Isolate a subband and then reconstruct the signal to focus on different spectral regions.
- The result is the low- and high pass filter.



- X-band fully polarimetric radar.
- Patch antenna transmits either horizontal or vertical polarisation, then receives both.
- Antenna is mounted underneath a Beech 1900C aircraft and can rotate 360°.
- Radar has a maximum bandwidth of 600 MHz, 1 kW transmit power.
- Azimuth two-way 3 dB beamwidth is $\sim 1^{\circ}$.
- Sea-clutter data has:
 - 200 MHz bandwidth / 0.75 m range resolution.
 - $\bullet~$ PRF is \sim 600 Hz.
 - Full-pol mode alternates horizontal and vertical transmit ? halves the effective PRF to \sim 300Hz.





Ingara Sea-Clutter

Dual polarised data with PRF of 575Hz; upwind direction; Douglas sea state: 4-5; grazing angles: 30.5° to 35.5° .

 HH polarisation: Horizontal transmitted and received data. Sea-spikes spread over a wide range of frequency (PSD iamges). It is chosen for our experimentation.



Data and Reconstructed Subband Analysis

Multiresolution analysis:

- Bandpass filter: the bandwidth of the decomposed signal is split in haft at each level.
- Combination: selections of bandwidths for filtering.





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Simulated stationary (lower) and moving (top) targets are injected to the data.

- Stationary target is always in *Ã_k* subband and appear brighter at lower resolution.
- Moving target is maintained in *D*₁.

Note: The subsequence detail subbands, \tilde{D}_2 and \tilde{D}_3 , has very little or no information about the targets for these type of target.



- Hypothesis test
 H₀: Interference (clutter + noise).
 H₁: Interference plus target.
- Probability of detection

$$P_d = \int_{\gamma}^{\infty} P_T(z) dz$$

Probability of false alarm rate

$$P_{\textit{fa}} = \int_{\gamma}^{\infty} P_{\textit{A}}(z) dz$$

 γ is the detection threshold.



A target with SIR of 10 dB is injected to all range bins. PDF of interference (int.) only and int. with a target are computed. Blue: int. only; Red: int. + stationary target; Black: int. + moving target.

- Stationary target: good PDF separation.
- Moving target: larger PDF separation.

The little information about the moving target is maintained in \tilde{A}_1 . It is reverse that no information about the stationary target is maintained in \tilde{D}_1 reconstructed subband.



Mean Separation of MRA

The target is now injected to all range bins and the 3-level multiresolution analysis (MRA) is investigated.

Target velocities: 0 m/s (stationary), 1.1 m/s and 2.6 m/s.

Mean separations show that:

- Stationary target: bigger mean separation at low resolution reconstructed subbands (*Ã_k*).
- Moving target: larger separation at higher detail resolution reconstructed subbands (*D*) and depending target velocity.



Subband Selection Based on Mean Separation

From the mean separations, we can select for the detection:

- Analysed subbands: $\tilde{A_1}, \tilde{D_1}, \tilde{A_2}, \tilde{D_2}, \tilde{A_3}, \tilde{D}_{12}, \tilde{D}_{23}$
- The method is good only if target velocities are know prior to the selection.



Determining the 'best' reconstructed subband to use for the detection. **Entropy** is a measure of information content in a set of measurements. For the random variable X, the entropy for the r^{th} range bin is:

$$H_r(X) = -\sum_n^N p_n \log(p_m/w_m)$$

where *N* is the number of bins for the histogram, p_n is the bin probability and w_n is the bin width.

- The entropy value varies with the variance or spreading of the histogram.
- To avoid the variation if the target is less or greater than the clutter

$$E_r(X) = \mid H_r(X) - \langle H \rangle \mid$$



The variation is greatly influenced by the target with SIR = 10 dB bin: 100.

Entropy Reconstructed Subband Indicator

The same Swerling-0 target is injected and maximum entropy of the analysed subbands are measured with target SIR is varied from -5 to 20 dB.

- Biggest increase found for:
 - Stationary A3
 - Moving 1.1 m/s target D₂₃
 - Moving 2.6 m/s target D₁
- These results match the mean separation results.
- Similar results found for Swerling 1 fluctuating target.

Entropy metric can be used as sub-band indicator.



Entropy Reconstructed Subband Indicator

The subband with the biggest maximum entropy is the subband with the most information about the target.

Subband maximum entropy:

 $\gamma_{subband} = max\{E_{subband}(X)\},\$

(subband: $\tilde{A_1}, \tilde{D_1}, \tilde{A_2}, \tilde{D_2}, \tilde{A_3}, \tilde{D_3}, \tilde{D}_{12}, \tilde{D}_{23}$)

- Proposed indication scheme using logic comparison on the same level SWT (Figure).
 - Faster computation.
 - Matching the mean separation (for the target with 10 dB SIR).



Detection Implementation

- Using HH upwind data of a CPI (128 pulse or 0.2 second).
- Swerling 0 (non-fluctuating) targets are injected with the SIR varied from 0 to 20 dB.
- Detection performance is quantified with Monte-Carlo simulation using 160 iterations with desired $P_{fa} = 10^{-3}$.
- Cell-Averaging CFAR (CA-CFAR) is used with local average over 32 range bins and with 2 guard bins.
- Threshold multiplier, *T*, is determined by K+Rayleigh model fit.



Three detection schemes are presented for the comparison:

- Conventional detection scheme.
- Detection of target with known velocity.
- Detection of target with unknown velocity and entropy sub-band indicator (eSWT).



Detection Comparison

Detection of Swerling 0 (non-fluctuating) target

- Detection results on left show improvements over the original range / time data of up to 7 dB for all targets (stationary and moving).
- Number of correctly chosen reconstructed subbands is shown on right as a function of SIR.
 - First two target cases have a transition around 3 dB.
 - Consistent result for fast moving target.



Detection of Swerling-1 Target

Swerling 1 target



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The stationary wavelet transform (SWT) - undecimated transform is investigated.

- We presented:
 - Isolates technique to reconstruct a subband of interest back to the range / time (data) domain.
 - MRA on the sea-clutter and its impact on the target by investigating the mean separation of each reconstructed sub-band.
 - Subband selection using an entropy metric which works for both stationary and moving targets.
 - Detection performance results showing a significant improvement over a conventional CA-CFAR of up to 7 dB.



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